

# Modeling the Thermal Performance of Phase Change Material Slurries (PCMS) in Laminar Falling Films

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**Abstract:** A Numerical model to investigate the heat transfer characteristic of a phase change material slurries (PCMS) flow over a cooled isothermal surface has been developed. The energy equation governs the heat transfer process includes the source term which accounts for the growth of the phase change material particles which are suspended in the heat transfer fluid to form of phase change materials slurries, PCMS. A fully developed velocity profile has been assumed to model the flow of thin constant falling film of suspensions. In this model the thermo-physical properties of the slurries are calculated based on their effective values which are function of phase change particles concentration. The main features of this work are that the phase change slurries show a binary behavior, i.e. they either in the frozen or melting state and are exposed directly to the water based solution without encapsulation. Parameters that influence the heat transfer characteristics are found to be the volumetric concentration of phase change suspensions, Nusselt number of the flow, PCM Nusselt number ( $NU_p$ ). The numerical results have showed that, heat transfer has been augmented due to the growth rate of phase change materials particles concentration.

**Keywords:** Falling Film, Flow of Suspensions, Heat Transfer, Phase Change

## 1. Introduction

It is well known that augmentation of heat transport can be achieved using slurry flow, especially if the dispersed particles involve a change of phase [7]. Several mechanisms responsible for this enhancement were examined, including particle rotation in shear flow, particles migration in laminar and turbulent flow, and the role of latent heat in increasing the heat transfer coefficient.

Recently phase change materials slurries in particular ice have been used extensively in energy storage, district cooling and control systems. The major attractive factors that make phase change material useful are (a) a high-energy storage density due the absorption or release of latent heat during the phase change process, (b) small temperature variation due to energy absorption at approximately constant temperature, (c) low pumping power requirements due to the increased heat capacity, (d) high heat transfer rates due to large ratio of surface area to the volume of the assumed spherical particles of the phase change suspensions. As a result a wide variety of applications have been suggested and implemented in practice [5]. Over the past decade several techniques of utilizing phase change material in energy storage and thermal control systems have been investigated [6]. In these techniques the phase change material is microencapsulated and suspended in a heat transfer fluid to form phase- change slurry.

With all the preliminary studies have concentrated on encapsulating the phase change material, as a heat transfer and storage medium, data for using phase change materials in binary fluids without encapsulating them had received little attention. A numerical model to approximate the rate of ice crystal growth on a cooled vertical plate has been proposed [14] to study the growth of ice particles suspended in a super-cooled liquid film, by regarding them as equivalent heat sources, distributed homogeneously in a water based solution. Fully developed fluid velocity was assumed in their analysis, the increase of particle size (concentration) and variable effective thermo physical properties of the slurry along the plate were considered. In their study, the effects of controlling parameters on heat transfer enhancement were also discussed.

In this paper, the thermal performance of phase change materials slurry flowing over a cooled isothermal surface is studied numerically. The numerical model is developed to include the phase change as a source term

in the governing energy equation, and uses small Stefan numbers to simulate some previous existing literature data as means of validation. The model is intended to investigate the thermal performance of phase change slurry for cool thermal energy storage applications.

## 2. Model Development

Several assumptions are used for the model shown schematically in Fig. 1, including incompressible laminar fully developed flow and spherically shaped particles of phase change materials. The fluid properties are assumed constant except for the effective values of thermal conductivity, viscosity, thermal diffusivity, and specific heat due to the interactions between the pcm particles and the host fluid. The flow is assumed Newtonian which is approximately the case for volumetric concentration of phase change material slurry less than 25 percent [11]. The phase change materials are assumed to be homogeneously distributed in the flow field and the densities of the fluid and pcm particles are assumed equal. Briefly, the model considers the pcm suspensions as well-dispersed heat sources in the falling film. Heat is transferred from the suspended pcm to the super cooled fluid and to the plate surface, and the subsequently generated solid phase (particle size increase) is maintained at the freezing temperature of the solution.

In the present study, the inlet temperature of the slurry was set at the initial freezing temperature of the solution, and axial diffusion is neglected in the governing energy equation. Only the constant temperature condition on the plate surface is considered here. Neglecting radiant and evaporative gains and losses, the governing equations and boundary conditions are:

The fully developed velocity profile [9] is:

$$u = \frac{ghy}{\nu_e} \left(1 - \frac{y}{2h}\right) \quad (1)$$

where  $u$  is constant in the lengthwise  $x$ - direction and  $v$ , perpendicular to the plate in the  $y$  direction, is assumed to be negligible. The governing steady state energy equation is:

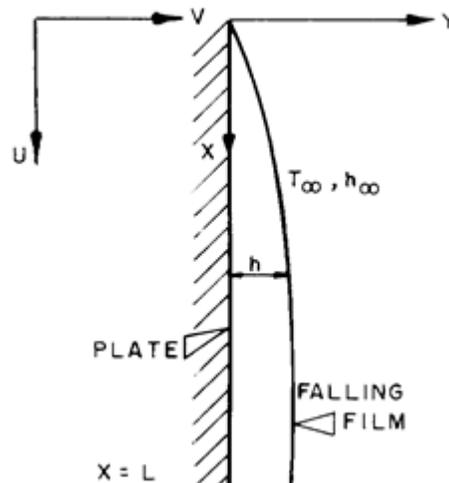


Fig.1 Falling Film Model of PCMS

$$\rho c_e u \frac{\partial T}{\partial x} = \frac{\partial}{\partial y} \left( k_e \frac{\partial T}{\partial y} \right) + S \quad (2)$$

The associated boundary conditions are:

$$T(x,0) = T_w, \quad (3)$$

$$T(0,y) = T_m = T_{in}, \quad (4)$$

$$k_e \frac{\partial T(x,h)}{\partial y} = h_{\infty} (T(x,h) - T_{\infty}) \quad (5)$$

Where,  $T_m$  and  $S$ , are the freezing temperature of the pcms and phase change source term, respectively.

Eq.(5) accounts for the convective heat transfer between the phase change material slurries and the surroundings. The effective bulk dynamic viscosity of the slurry is assumed to be a function of ice crystal volumetric concentration,  $C$ , (Stewart et al. 1993) as

$$\frac{\mu_b}{\mu_f} = (1 - C - 1.18C^2)^{2.5}; \quad C \leq 0.45 \quad (6)$$

and the effective kinematic viscosity is defined as

$$v_e = \frac{\mu_b}{\rho} \quad (7)$$

The effective specific heat,  $c_e$ , is defined as the mass or volume averaged specific heats of the pcm particles and fluid:

$$c_e = Cc_p + c_f(1-C) \quad (8)$$

Where  $c_p$  and  $c_f$  are the particle and fluid specific heats, respectively. The effective thermal conductivity,  $k_e$ , is related to the bulk fluid thermal conductivity by the relation

$$\frac{k_e}{k_b} = 1 + B C Pe_p^m \quad (9)$$

where the constants,  $B$  and  $m$ , have the assigned values of 1.8 and 0.18, respectively, based on the work of [13] and [3] for moderate to large Peclet numbers.

The source term,  $S$ , of equation 2 can be represented as:

$$nQ_{pcm} = \rho h_{if} u \left( \frac{n\pi}{2} \right) d^2 \frac{\partial d}{\partial x} \quad (10)$$

$$\frac{\partial d}{\partial x} = \frac{2h_d(T_m - T)}{\rho h_{if} u} \quad (11)$$

The local concentration,  $C$ , is defined as

$$C = n \frac{\pi d^3}{6} \quad (12)$$

### 3. Solution Methodology

Finally, by defining the following dimensionless variables

$$\begin{aligned} X &= \frac{x}{L}, & Y &= \frac{y}{h}, & D &= \frac{d}{h}, \\ V &= \frac{u}{u_{y=h}}, & \phi &= \frac{T - T_w}{T_{in} - T_w}, & \Gamma &= \frac{k_e}{k_b} \end{aligned} \tag{13}$$

Eqs. (1) - (5), eqs.(11), and (12) become

$$V = 2Y - Y^2 \tag{14}$$

$$\frac{\partial}{\partial X}(\rho V \phi) = \frac{\partial}{\partial X}(\eta \Gamma \frac{\partial \phi}{\partial X}) + \frac{L^2}{h^2} \frac{\partial}{\partial Y}(\eta \Gamma \frac{\partial \phi}{\partial Y}) + S \tag{15}$$

$$\phi(X, 0) = 0 \tag{16}$$

$$\phi(0, Y) = 1 \tag{17}$$

$$\left(\frac{\partial \phi}{\partial Y}\right)_{Y=1} = \frac{h_\infty \cdot h}{\Gamma} (\phi_{Y=1} - \phi_\infty) \tag{18}$$

$$\frac{\partial D}{\partial X} = \frac{2 Ste L}{\rho V u_h h c_f} h_d (\phi_m - \phi) \tag{19}$$

$$C = \frac{n \pi h^3}{6} D^3 \tag{20}$$

where

$$\begin{aligned} \eta &= \frac{1}{V_h \cdot L \cdot c_e} ; Ste = \frac{c_f (T_{in} - T_w)}{h_{if}} \\ \Gamma &= 1 + BC 2^m (Pe_f (1 - y))^m d^{2m} \end{aligned} \tag{21}$$

$$S = \frac{\rho V}{Ste} \frac{c_f}{c_e} \frac{\partial C}{\partial X} ; \frac{\partial C}{\partial X} = \left(\frac{n \pi h^3}{2}\right) D^2 \frac{\partial D}{\partial X} \tag{22}$$

The heat transfer coefficient,  $h_d$ , between the pcm and the fluid was determined using the natural convection correlation for spheres as a particle Nusselt number,  $Nu_p$ ,

$$Nu_p = 2 + 0.5 Ra^{0.25} \tag{23}$$

(a) The local plate (wall) Nusselt number is defined as

$$Nu_x = \frac{h_x x}{k_e} \tag{24}$$

where,  $k_e$ , is the effective thermal conductivity of the mixture near the plate surface.

(b) The local heat transfer coefficient is evaluated as

$$h_x = \frac{q_w}{T_w - T_m} \quad (25)$$

(c) The heat transfer at the wall is defined as

$$q_w = \frac{k_e(T_w - T_{i,2})}{\Delta y} \quad (26)$$

where  $T_{i,2}$  is the fluid temperature at the control volume next to the wall.

(d) The overall heat transfer coefficient is calculated as

$$U = \frac{1}{L} \int_0^L h_x dx \quad (27)$$

where,  $L1$  and  $M1$  are the number of nodes in the  $x$  and  $y$  directions respectively.

Since the source term in the governing energy equation, eq. (15), is an implicit function of the slurry temperature, the axial and vertical coordinate, and particle diameter distribution, no analytical solution exists and, therefore, a steady-state control-volume finite-difference approach described by [12] was used to predict the dimensionless temperature,  $\phi$ , from eq. (15) and pcm particle diameter from eq. (19) throughout the flow field at steady-state conditions. The solution was considered complete when the change in  $\phi$  values upon subsequent iterations was less than  $10^{-6}$ . In this solution methodology the discretized forms of eqs. (15) - (19) are obtained by applying the conservation laws over a finite control volume surrounding each grid node and integrating over the control volume. The harmonic mean of thermal conductivity is used at the control volume faces. The sequence of numerical calculations is identical to that used to solve conventional single-phase problems. The Coupling that exists between the energy and pcm particle diameter equations is accommodated through iteration, and under relaxation. Within the iterative scheme, eqs. (15) - (20) provide necessary descriptions of the temperature fields, as well as the concentration distributions for the evaluation of the effective values of the thermal conductivity, thermal diffusivity, kinematic viscosity, and the specific heat. Supplementary numerical calculations performed on grids ranging from  $20 \times 20$  to  $75 \times 75$  suggested that satisfactory grid independence could be achieved using a  $50 \times 50$  grid.

The film thickness in the  $y$  direction was modeled as 0.5 mm, 0.75 mm, and 1.0 mm corresponding to a Reynolds of 137, 451, and 1058, respectively. A constant plate length of 1.0 m was used for all simulations. The inlet diameter of each pcm particle,  $d_{in}$ , was 0.025 mm to initialize the calculations. Assuming there are 2500 particles for each 0.1 mm of film thickness per 1 m<sup>2</sup> of plate surface area, there are  $2.5 \times 10^7$  pcm particles per m<sup>3</sup> of film. The inlet temperature was set at the initial freezing point temperature of the solution, but the freezing point temperature decreases as the concentration of pcms increases during growth in the  $x$ - direction. At the film free surface (boundary), the heat transfer coefficient,  $h_\infty$ , was assumed as 10 w/m<sup>2</sup>k. The freezing (melting) temperature of the solution,  $T_m$ , is a function of pcm particle concentration [2]. The relationship between pcms concentration and freezing (melting) temperature of the solution was assumed as a polynomial relationship of the form

$$T_m = a_0 + a_1C + a_2C^2 \quad (28)$$

where the coefficients,  $a_i$ , are calculated from the phase diagram of NaCl-H<sub>2</sub>O system [4]. The continuum formulation and numerical predictions of the present model have been verified through comparison with

literature results [14] for the special case of negligible axial diffusion. As a check of the precision of the numerical model, a heat balance was performed for each simulation. The heat balance is between the calculated heat flux at the plate surface and the sum of the heat fluxes from sensible cooling of the film, the latent heat flux from ice growth, and the convective heat flux from the surroundings at the film free surface. In equation form the heat balance is

$$Q_w = \dot{m} c_f (T(x, y) - T_{in}) + \rho V_{crystal} h_{if} \frac{\partial c}{\partial t} + h_{\infty} A_{\infty} (T(x, h) - T_{\infty}) \quad (29)$$

## 4. Results

The solutions are presented in terms of the dimensionless particle diameter, concentration profiles, local (wall) Nusselt number, for different isothermal plate temperature (Stefan number), and film thickness. The concentration profiles along the plate length,  $x$ , in the film for the case of  $T_w = 267$  K,  $T_{in} = 271$  K, ( $Ste = 0.05$ ),  $h = 0.5$  mm, and  $d_{in} = 0.05$  mm are shown in Fig. 2, indicating naturally the greatest increase near the surface of the plate as was expected. Figure 3 shows the dimensionless pcm particle diameter distribution across the film thickness and for three axial positions along the vertical plate. The figure indicates large increase in the dimensionless pcm particle diameter near the cold plate wall and for large axial positions along the plate. Figures 4 depicts the variation of local (wall) Nusselt number along the axial coordinate for different film thickness and constant plate temperature conditions. It is noted that, the local Nusselt number increases with increasing distance along the plate,  $x$ , and decreases with increasing film thickness. The effect of film thickness on local Nusselt number at different elevations is shown in Fig. 5. The decrease of local Nusselt number with film thickness can be attributed to the decrease of pcm diameter (concentration) for larger film thickness, that is, the sensible heat flux is greater than the latent heat flux, and the resultant mass growth rates decrease with increasing film thickness. Fig. 6. Demonstrate the effect of Stefan number on the PCMS concentrations and hence on the particle size growth.

The numerical results are very sensitive to the equation governing the particle growth within the film. The growth of pcm particles was related to the degree of supercooling of the fluid, which is increased as the film flows down the plate. A rate equation that may reflect the actual, experimental growth rate of an ice particles subject to different supercoolings may significantly affect the results reported here. Also consideration of nucleation and agglomeration of micro suspensions which are not modeled here may further affect the numerical results of the present model. At present there is no available experimental data for growth rates under similar conditions.

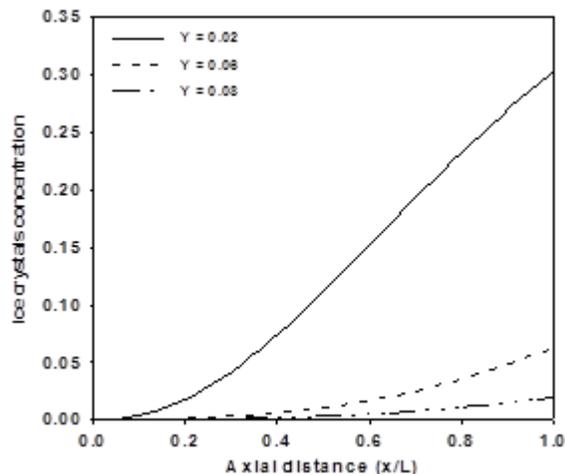


Fig. 2. PCMS concentration variation,  $C$ , with axial distance

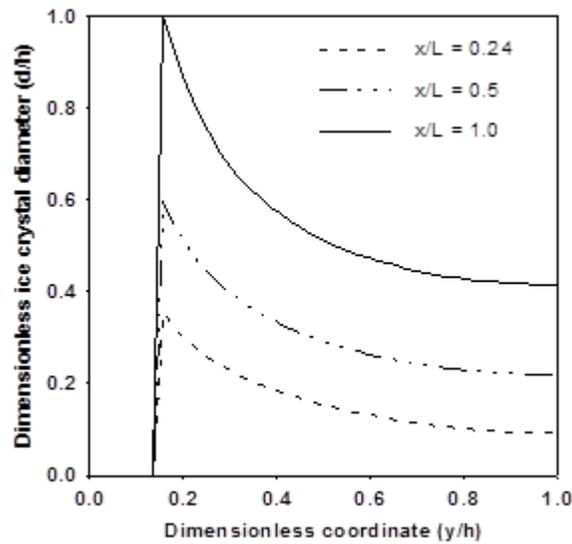


Fig. 3. Particles size (diameter) variation with Y-coordinate at different X-locations

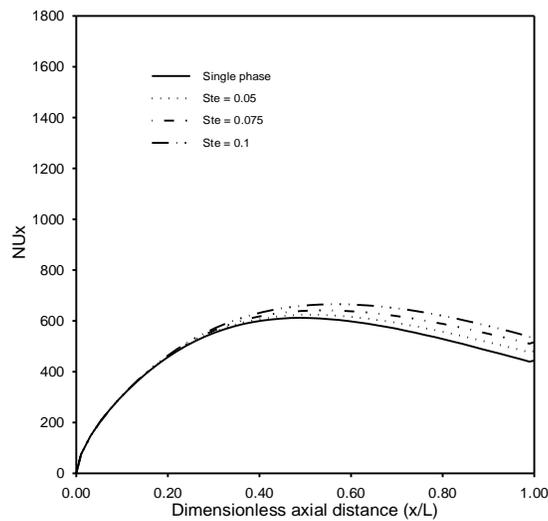


Fig. 4. Nusselt number variation at the plate surface with plate length

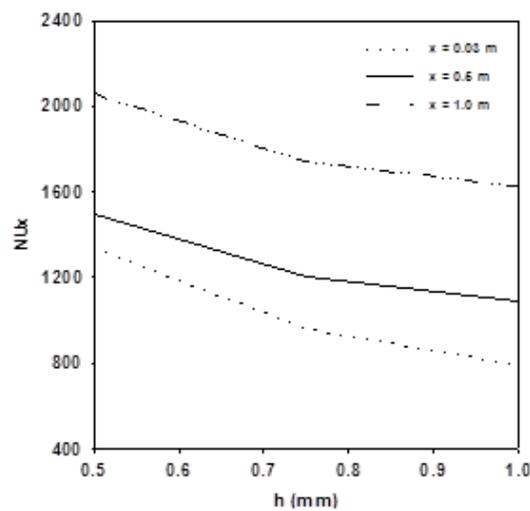


Fig. 5. Effect of film thickness,  $h$ , on local Nusselt number at the plate surface for different X elevation

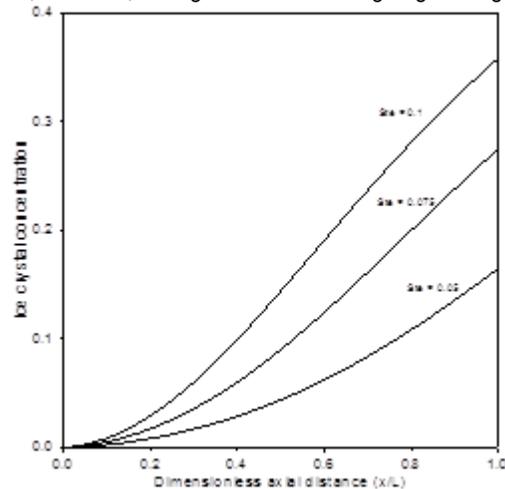


Fig. 6. Effect of Stefan number on the phase change material concentration

## 5. Conclusion

A numerical model has been developed to study thermal performance of phase change material slurries. The numerical results showed that pcm particle growth rate appears to be primarily a function of Stefan number and film thickness (mass flow rate). Nusselt number. Results have showed that phase change material slurries can effectively enhance the heat transfer coefficient and sustain the fluid temperature. Such enhancement of heat transfer coefficient may be utilized in the effective control of surface temperature (wall), and flow rate reduction. Results of the over all heat transfer coefficient showed that heat transfer can be augmented up to 12 % in the case of using phase change material slurries as a heat transfer fluid. Comparative calculations were performed for different film thicknesses to assess the effect of including axial diffusion in the governing energy equation; it was found that axial diffusion effects were more pronounced (increase of Nusselt number) for the 0.5 mm and 0.75 mm film thickness and has less influential effect for larger film thicknesses. In summary, the present results have given promises of utilizing PCMS as a heat transfer fluid.

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